

WRS10/12/58

Notes on Auxiliary Power Pack and Relay
for :

25X1

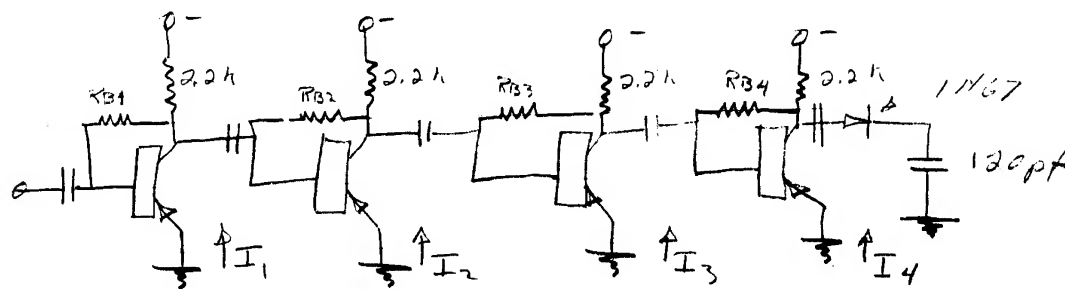
1. Wire both audio leads directly to external terminal block.
2. The recorder that is used in place of the Minfon will have its own power.
3. Our 15-volt supply (sitmarcel) need not be brought out to terminal block.
4. The relay ^{coil} will not be brought out to the terminal block.
5. Bring ground or common to terminal block.

6. Package configuration: Two rows of five cells each with plug, relay and terminal block on end if practical.

NK6.
Not included

This document is part of an integrated file. If separated from the file it must be subjected to individual security review.

NCP

23 May 1956VIDEO AMPLIFIER

Gain: $100 \mu\text{V}$ to $.8 \text{ volts}$ at 80 kc

Bandwidth: $\sim 380 \text{ kc}$

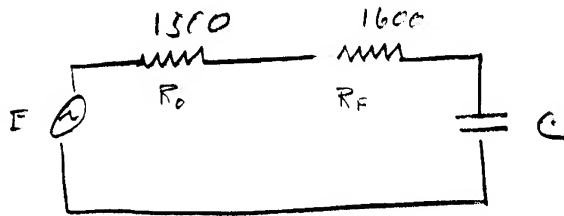
Output impedance of final stage - 1500Ω

$R_{B1} = R_{B2} = R_{B3} = 250 \text{ k to } 500 \text{ k}$

$R_{B4} \approx 165 \text{ k}$



Pulse stretcher:



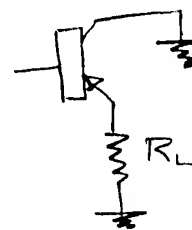
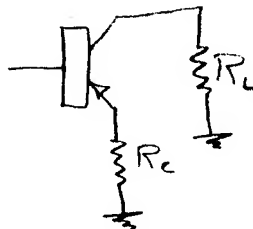
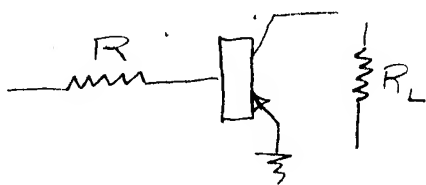
R_F : forward resistance of 1N67 at .25 volts = 1600Ω

R_o output resistance of video amp = 1500Ω

Capacity of pulse stretcher

$$\omega_0 C = -\frac{1}{R_o + R_F} \quad (\omega_0 = 2\pi \times 380 \text{ Kc})$$

$$C = 130 \mu\mu\text{F}$$



APPROXIMATE

$$R_i: R + r_b + \frac{r_e}{1-a}$$

$$A_v: - \frac{r_b + \frac{r_e}{1-a}}{R + r_b + \frac{r_e}{1-a}} \cdot \frac{a R_L}{r_e + r_b(1-a)}$$

$$= - \frac{a}{1-a} \frac{R_L}{R_i}$$

$$R_i + \frac{R_E + r_e}{1-a}$$

$$= - \frac{a R_L}{R_E + r_e + r_b(1-a)}$$

$$= - \frac{a}{1-a} \frac{R_L}{R_i}$$

$$\frac{R_L}{1-a}$$

$$= \frac{1}{1-a} \frac{R_L}{R_i}$$

R_i and thus R_i , may be greatly increased without affecting the approximate formulas

The higher approximate formula has $(R_E + r_e)$ appearing in the denominator of A_v . - Thus for large values of R_E , the voltage gain will be less.

As R_L is increased R_i reaches the limit of r_e while A_v remains constant.

This document is part of an internal
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ACS 12 June 1956

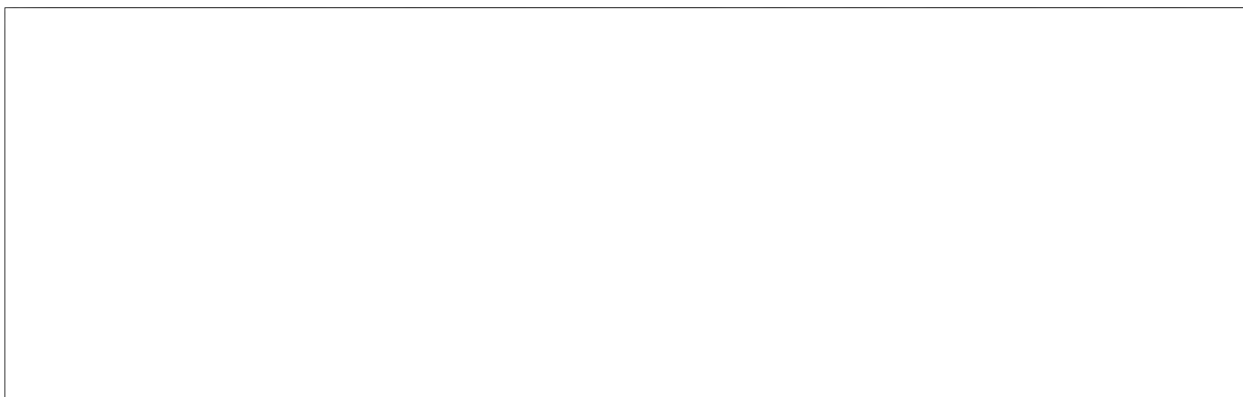
Shea pp 62.63

13 July 1956

PROPOSED IMPROVEMENTS ON DEMAND SYSTEM

The following improvements are suggested for optimizing the crystal video demand receiver:

1. Incorporate Philco video amplifier and pulse stretcher for good short pulse response.



25X1

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BIAS STABILIZED

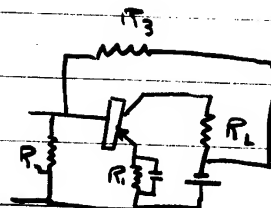
AUDIO AMPLIFIER

ACS

22 Feb 1956

I. The stability factor (S) is given by Shea as:

$$S = \frac{1 + R_1/R_2 + R_1/R_3}{1 - \alpha + R_1/R_2 + R_1/R_3}$$

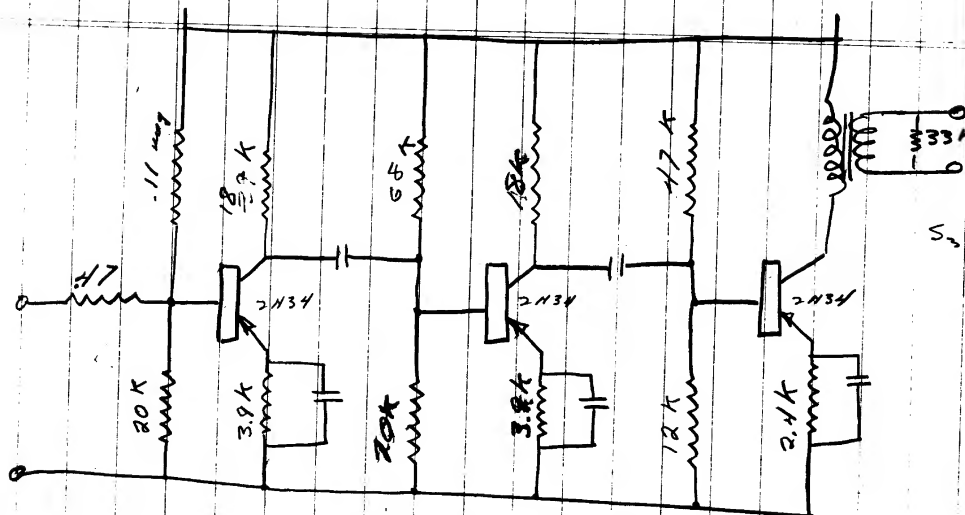


So for the circuit shown:

Stage	Stability factor	$\frac{I_{CQ}}{I_{CQ0}}$
1	4.8	
2	4.53	
3	4.53	

II. Measurements of gain vs temperature indicated that the values of bias resistance are much more critical during a change in temperature.

A change of the order of magnitude of a few degrees centigrade per minute is sufficient to cause a noticeable decrease in gain (several db).



$$S_1 = \frac{1 + .195 + .035}{.025 + .195 + .035} = \frac{1.225}{.255} = 4.8$$

$$S_2 = \frac{1 + \frac{.195}{20} + \frac{.057}{68}}{\frac{1}{40} + \frac{.195}{20} + \frac{.057}{68}} = 4.53$$

$$S_3 = \frac{1 + .200 + .051}{.025 + .200 + .051} = \frac{1.251}{.276} = 4.53$$

$$\frac{1.252}{.277}$$

$$\frac{.025}{.195} = .057$$